TEXT SEARCHABLE DOCUMENT - 2010

DATA EVALUATION RECORD

STUDY 3

CHEM 031401

Dichloroprop

§163-1

CAS No. 15165-67-0

FORMULATION--00--ACTIVE INGREDIENT

STUDY ID 44028901

Wells, D. F. 1996. 2,4-DP-p: determination of batch-equilibrium adsorption and desorption coefficients following FIFRA guideline §163-1. Laboratory Project No. 13021.0495.6105.710. Unpublished study performed by Springborn Laboratories, Inc., Wareham, MA; and submitted by 2,4-DP Task Force, Research Triangle Parkway, NC.

DIRECT REVIEW TIME = 55 Hours

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DATA EVALUATION RECORD

STUDY 3

CHEM 031402

Dichloroprop

§163-1

CAS No. 15165-67-0

FORMULATION--00--ACTIVE INGREDIENT

STUDY ID 44028901

Wells, D. F. 1996. 2,4-DP-p: Determination of batch-equilibrium adsorption and desorption coefficients following FIFRA guideline §163-1. Springborn Study No.: 13021.0495.6105.710. Unpublished study performed by Springborn Laboratories, Inc., Wareham, MA; and submitted by the 2,4-DP Task Force, Research Triangle Parkway, NC.

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acetone), at nominal concentrations of 1.2, 0.60, 0.30, and 0.15 mg/L, were added to glass centrifuge tubes containing samples (8 g) of air-dried, sieved (2 mm) clay, sand, sandy loam, and Timmerman sandy loam soils; triplicate tubes were prepared for each soil type/treatment rate combination (p. 17). The soil:solution slurries (1:5, w:v) were mechanically shaken for 18 hours at 20 ± 2 °C (pp. 13, 17). Control tubes without soil containing treated CaCl₂ solution were equilibrated along with the sample soil:solution slurries. Following the equilibration period, samples were centrifuged and the supernatant was decanted. Aliquots of the supernatant from each sample were analyzed for total radioactivity by LSC (pp. 14, 18); the detection limit was 0.58 μ g/L (p. 15).

For the desorption phase of the study, pesticide-free 0.01 M CaCl₂ solution (5 mL less than recovered in the adsorption phase) was added to the centrifuge tubes containing soil from the adsorption phase of the study (p. 25; see Comment #2). The samples were shaken for 48 hours and maintained as previously described. Following the equilibration period, samples were centrifuged and the supernatants were decanted. Aliquots of the supernatant from each sample were analyzed for total radioactivity by LSC. An additional desorption was conducted for the clay and sandy loam soils. Following the initial desorption phase, additional pesticide-free CaCl₂ solution was added to the two soils and the samples were shaken for 18 hours. Following the equilibration period, the samples were centrifuged and the supernatant was decanted. Aliquots of the supernatant were analyzed for radioactivity by LSC. The post-extracted clay and sandy loam soils were analyzed for total radioactivity by LSC following combustion.

An independent stability test was conducted to determine if the parent compound was stable under test conditions (p. 15). Aliquots of 0.01 M CaCl₂ solution treated with uniformly phenyl ring-labeled [¹⁴C]dichloroprop, at a nominal concentration of 1.20 mg/L, were added to three glass centrifuge tubes containing samples of each soil. The soil:solution slurries (1:5, w:v) were mechanically shaken for 36 hours and the supernatant was decanted (p. 16). Aliquots of the supernatant were analyzed by reverse-phase HPLC (Metachem Spherisorb ODS-2 column) using a mobile phase gradient of 0.1% trifluoroacetic acid (in reagent water):acetonitrile (60:40 to 40:60 to 0:100, v:v) with radioactive flow detection; samples were co-chromatographed with nonradiolabeled reference standards (pp. 16, 17). The data indicated that the parent compound was stable; 96.6-100% (based on individual replicates for all soils) of the recovered radioactivity was present as parent (Table III, p. 31).

DATA SUMMARY

Uniformly phenyl ring-labeled [14 C]dichloroprop (radiochemical purity 98.3%), at nominal concentrations of 1.2, 0.60, 0.30, and 0.15 mg/L, was studied in clay, sand, and two sandy loam soil:solution slurries (1:5, w:v) that were equilibrated for 18 hours at 20 \pm 2 °C. Freundlich K_{ads} values were 0.79 for the clay soil, 0.25 for the sand soil (see

Comment #4), 1.7 for the sandy loam soil (3.5% o.m.), and 0.41 for Timmerman sandy loam soil (0.9% o.m.; Tables V, VII, IX, XI, pp. 33, 35, 37, 39); corresponding K_{oc} values were 83.7, 32.7, 81.5, and 78.2 mL/g. Respective 1/N values were 0.87, 0.59, 0.84, and 0.91 for adsorption. The reviewer-calculated coefficient of determination (r^2) values for the relationships K_{ads} vs. organic matter, K_{ads} vs. pH and K_{ads} vs. clay content were 0.92, 0.48 and 0.002, respectively. Freundlich K_{des} values determined after a 48-hour equilibration period were 1.3 for the clay soil, 0.17 for the sand soil, 3.1 for the sandy loam soil, and 2.5 for Timmerman sandy loam soil (Tables VI, VIII, X, XII, pp. 34, 36, 38, 40); corresponding K_{oc} values were 143, 21.9, 149, and 474 mL/g. Respective 1/N values were 0.59, 0.28, 0.72, and 0.84 for desorption.

During the 18-hour equilibration period, 13.7-17.3% of the applied radioactivity was adsorbed to the clay soil (across all application levels), 4.1-9.7% was adsorbed to the sand soil, 25.0-32.4% was adsorbed to the sandy loam soil, and 6.9-9.4% was adsorbed to the Timmerman sandy loam soil (Table IV, p. 32). Following a single desorption, 5.8-36.6% of the previously adsorbed radioactivity was desorbed from the clay soil (across all application levels), 32.4-103% was desorbed from the sand soil, 18.7-32.9% was desorbed from the sandy loam soil, and 4.7-15.7% was desorbed from the Timmerman sandy loam soil.

The stability of the parent compound in the soil:solution slurries following the adsorption and desorption phases was not confirmed; [14C]residues were not characterized (see Comment #1).

Material balances (based on LSC analysis of individual replicates) across all application rates were 97.1-104.4% for the Arkansas clay soil samples, 92.7-101% for the Georgia sand soil samples, 95.5-100% for the sandy loam soil samples, and 90.6-94.7% for the Timmerman sandy loam soil samples (Tables XIII-XVI, pp. 41-44).

COMMENTS

- 1. It could not be confirmed that the parent compound was stable throughout the definitive study; [14C]residues in the desorption supernatant were not characterized. Data from an independent stability study indicated that the parent compound was stable following a 36-hour adsorption period; 96.6-100% of the applied radioactivity was parent (Table III, p. 31). A desorption phase was not conducted in the independent stability study.
- 2. For the desorption phase of the definitive study, the amount of pesticide-free 0.01 M CaCl₂ added to the soil remaining from the adsorption phase was 5 mL less than the volume decanted following the adsorption phase. The study author stated that the volumes added were inadvertently 5 mL less because the volume of the solution removed for analysis following the adsorption phase was accounted for (p. 25).

- 3. The soil series names for three of the soils used in the study were not reported.
- 4. Only three concentrations were used to plot the desorption isotherm for the sand soil (Figure 11, p. 56). The study author stated that the results from the highest concentration (1.2 mg/L) were omitted from regression analysis due to the low levels of residues calculated to be in the soil (p. 22). At least four concentrations are necessary to accurately determine Freundlich isotherms and K_{ads/des} values.
- 5. Method detection limits were reported for LSC analysis, but were not reported for HPLC analysis. Both limits of quantitation and detection should be reported to allow the reviewer to evaluate the adequacy of the test method for the determination of the test compound.
- 6. It could not be determined whether one of the soils used in the study was the same type of soil used in the aerobic metabolism study.
- 7. The study author did not indicate whether the definitive study was conducted in darkness; however, the test containers were placed in an environmental chamber (p. 13). The study author stated that the preliminary study was conducted in darkness.
- 8. The study author stated that, after LSC analysis of the aqueous desorption solution, adequate material balances for the sand and Timmerman sandy loam soils was obtained; therefore, these soils were not combusted to determine bound residues (p. 18).

Table I. Soil characteristics of Arkansas clay, Georgia sand, Sandy Loam and Timmerman sandy loam.

| Soil Characteristics | s (0 to 9 inches) | Arkansas | Georgia | Sandy Loam | Timmerman |
|----------------------|-------------------|----------|---------|------------|------------|
| Classification | | Clay | Sand | Sandy loam | Sandy loam |
| % Sand | | 16 | 92 | 56 | 66 |
| % Silt | | 34 | 2 | 36 | 27 |
| % Clay | | 50 | 6 | 8 | 7 |
| % Organic | | | | | |
| Matter | | 1.6 | 1.3 | 3.5 | 0.9 |
| % Organic | | | | | |
| Carbon ^a | | 0.941 | 0.765 | 2.06 | 0.529 |
| ~11 | | 7.0 | 0.7 | 0.0 | ~ . |
| pН | | 7.0 | 6.7 | 6.3 | 7.4 |
| Bulk Density | | | | | |
| (disturbed) g/cc | | 1.09 | 1.35 | 0.94 | 1.28 |
| Cation Exchange | | | | | |
| Capacity (meq/100 g | 3) | 34.9 | 4.3 | 11.9 | 14.4 |
| Exchangeable | | | | | |
| Cations (ppm) | | | | | |
| · · · · | Calcium | 61.6 | 47 | 29.4 | 58.9 |
| | Magnesium | 25.3 | 19.6 | 14 | 19 |
| | Sodium | 1.3 | 1.8 | 0.9 | 0.7 |
| | Potassium | 2.2 | 1.4 | 3.8 | 5.9 |
| | Hydrogen | 9.6 | 30.1 | 51.8 | 15.5 |
| Field Moisture | | | | | |
| Capacity at 1/3 Bar | (%) | 30 | 7.3 | 39.1 | 12.5 |

Soil analysis was performed by Agvise Laboratories, Northwood, North Dakota.

^a Calculated from % organic matter using the formula: % organic carbon = % organic matter/1.7. (Black *et al.*, 1965)

Table II. Measured concentrations of 2,4-DP-p concentrations during the preliminary (equilibrium determination) test.^a

| Time (Hours) | Concentration (mg/L) ^b | Time (Hours) | Concentration (mg/L) ^b | |
|-----------------|--------------------------------------|-----------------|--------------------------------------|--|
| ARKAI | ISAS | GEO | PRGIA | |
| 5 | 1.09 | 5 | 1.13 | |
| 18 ^c | 1.04 | 18 ^c | 1.14 | |
| 24 | 1.05 | 24 | 1.09 | |
| SAND | LOAM | TIMI | MERMAN | |
| 5 | 0.943 | 5 | 1.11 | |
| 18 ^c | 0.939 | 18 ^c | 1.15 | |
| 24 | 0.898 | 24 | 1.12 | |

Calculated values are based on unrounded data rather than the rounded numbers presented here.

Apparent errors in calculation may result from using rounded values.

b Initial concentration was 1.2 mg/L.

Time selected for equilibration of 2,4-DP-p with this soil.

Table III. Stability of 2,4-DP-p as determined by HPLC-RAM after 36 hours of shaking.

| | Sample ID | % of Initial Radioactivity in Aqueous Portion ^a | Measured Concentration (mg/L) ^a | Radioactivity Distribution (% Parent) |
|-------------------------|----------------------------|--|--|---|
| | | Arkansas clay | | |
| Arkansas Clay | Rep. 1 Rep. 2 Rep. 3 | 90.9 87.1 87.1 | 1.07 1.02 1.02 | 100 100 100 |
| | | Georgia sand | | |
| Georgia Sand | Rep. 1 Rep. 2 Rep. 3 | 91.1 91.5 94.2 | 1.07 1.08 1.11 | 100 100 100 |
| | | Sandy loam | | |
| Sandy Loam | Rep. 1 Rep. 2 Rep. 3 | 73.8 70.7 72.7 | 0.867 0.831 0.850 | 100 100 97.8 |
| | | Timmerman sandy loam | | |
| Timmerman Sandy Loam | Rep. 1 Rep. 2 Rep. 3 | 89.8 96.8 91.2 | 1.06 1.14 1.07 | 100 100 96.6 |

^a Determined by Liquid Scintillation Counting (LSC).

^b Determined by HPLC-RAM. Initial concentration prior to equilibration was 1.2 mg/mL.

Table IV. Summary of mean adsorption and desorption results from isotherm tests for 2,4-DP-p.^{a,b}

| | | Adsorption | | D | esorption | |
|-----------|---------|------------|-------|-------------------|-----------|------|
| Soil-Less | Aqueous | Soil | | Aqueous | Soil | |
| Control | Conc. | Conc.c | | Conc. | Conc.c | |
| (mg/L) | (mg/L) | (mg/kg) | %Ads. | (mg/L) | (mg/kg) | %Des |
| | | | | | | |
| | | | | sas clay | | |
| 1.22 | 1.05 | 0.835 | 13.7 | 0.178 | 0.560 | 33.2 |
| 0.620 | 0.531 | 0.443 | 14.3 | 0.0947 | 0.283 | 36.6 |
| 0.309 | 0.260 | 0.247 | 16.0 | 0.0410 | 0.192 | 22.0 |
| 0.156 | 0.129 | 0.135 | 17.3 | 0.0161 | 0.127 | 5.78 |
| | | | Georg | gi <u>a sand</u> | | |
| 1.22 | 1.17 | 0.252 | 4.14 | 0.110 | 0.0190 | 103 |
| 0.620 | 0.579 | 0.207 | 6.67 | 0.0573 | 0.0790 | 61.8 |
| 0.309 | 0.285 | 0.118 | 7.66 | 0.0280 | 0.0567 | 53.2 |
| 0.156 | 0.141 | 0.076 | 9.74 | 0.0126 | 0.0515 | 32.4 |
| | | | Sar | idy loam | | |
| 1.22 | 0.912 | 1.52 | 25.0 | 0.212 | 1.02 | 32.9 |
| 0.620 | 0.444 | 0.882 | 28.4 | 0.107 | 0.624 | 29.4 |
| 0.309 | 0.217 | 0.462 | 29.9 | 0.0500 | 0.345 | 25.3 |
| 0.156 | 0.105 | 0.253 | 32.4 | 0.0223 | 0.205 | 18.7 |
| | | | Tim | merman sandy loam | | |
| 1.22 | 1.13 | 0.417 | 6.85 | 0.104 | 0.359 | 13.2 |
| 0.620 | 0.562 | 0.290 | 9.35 | 0.0553 | 0.245 | 15.7 |
| 0.309 | 0.283 | 0.130 | 8.41 | 0.0267 | 0.113 | 14.1 |
| 0.156 | 0.143 | 0.0673 | 8.63 | 0.0124 | 0.0636 | 4.71 |

^a Calculated values are based on unrounded data rather than the rounded numbers presented here. Apparent errors in calculation may result from using rounded values.

Test solutions were prepared with theoretical concentrations of 1.20, 0.600, 0.300, and 0.150 mg/L. Measured solution concentrations (LSC) prior to addition to soil were 1.24, 0.628, 0.315, and 0.160 mg/L, repectively.

^c Calculated from aqueous concentration.

Table V. Measured aqueous concentrations, calculated soil concentrations and linear regression results for adsorption of 2,4-DP-p to Arkansas Clay during isotherm testing

| | | | | |
|---|---|---|---|---------------------------------------|
| Initial | Measured Aqueous | Calculated So | · - · | |
| Concentration ^a | Concentration | Concentration | ו | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.22 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 1.03 1.06 1.06 1.05 0.0130 | 0.910 0.795 0.800 0.835 0.0650 | | |
| 0.620 mg/L | | | LOG (Ce) | LOG (Cs) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.561 0.518 0.515 0.531 0.0257 | 0.295 0.510 0.525 0.443 0.129 | 0.0208 -0.275 -0.586 -0.889 | -0.0783 -0.353 -0.608 -0.870 |
| 0.309 mg/L Replicate 1 Replicate 2 | 0.265 0.253 | 0.220 0.280 | Slope (1/n) Y-intercept (log K) Coefficient of Determination (r²) | 0.865 -0.104 0.999 |
| Replicate 2 Replicate 3 Mean Standard Deviation | 0.261 0.260 0.00611 | 0.240 0.247 0.0306 | ` , | 1.16 |
| 0.156 mg/L | | | n K Koc | 0.788 83.7 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.130 0.130 0.127 0.129 0.00167 | 0.130 0.130 0.144 0.135 0.00837 | | |

^a Concentration in soil-less control

Table VI. Measured aqueous concentrations, calculated soil concentrations and linear regression results for desorption of 2,4-DP-p from Arkansas clay during isotherm testing.

| Initial | Measured Aqueous | Calculated So | <u> </u> | |
|---|--|---|---|--------------------------------------|
| Concentration ^a | Concentration | Concentration | | |
| | (mg/L) | (mg/kg) | • | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.22 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.170 0.178 0.185 0.178 0.00751 | 0.662 0.523 0.496 0.560 0.0894 | | |
| 0.620 mg/L | | | LOG (C ₁) | LOG (Cd) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0880 0.0980 0.0980 0.0947 0.00577 | 0.180 0.328 0.341 0.283 0.0899 | -0.750 -1.02 -1.39 -1.79 | -0.252 -0.548 -0.717 -0.896 |
| 0.309 mg/L Replicate 1 Replicate 2 | 0.0410 0.0440 | 0.168 0.208 | Slope (1/n) Y-intercept (log K) Coefficient of Determination (r²) | 0.590 0.128 0.951 |
| Replicate 3 Mean Standard Deviation | 0.0380 0.0410 0.00300 | 0.199 0.192 0.0213 | n | 1.70 |
| 0.156 mg/L | | | K'oc | 1.34 143 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0154 0.0169 0.0159 0.0161 0.000764 | 0.126 0.119 0.136 0.127 0.00885 | | |

^a Concentration in soil-less control

Table VII. Measured aqueous concentrations, calculated soil concentrations and linear regression results for adsorption of 2,4-DP-p to Georgia sand during isotherm testing.

| Intial Concentration ^a (mg/L) | Measured Aqueous Concentration (mg/L) | Calculated So Concentration (mg/kg) | ••• | |
|---|---|---|---|-------------------------------------|
| 1.22 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 1.14 1.17 1.18 1.17 0.0202 | 0.360 0.235 0.160 0.252 0.101 | | |
| 0.620 mg/L | | | LOG (Ce) | Log (Cs) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.578 0.578 0.580 0.579 0.00115 | 0.210 0.210 0.200 0.207 0.00577 | 0.0666 -0.238 -0.545 -0.851 | -0.599 -0.685 -0.927 -1.12 |
| 0.309 mg/L Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.283 0.282 0.291 0.285 0.00493 | 0.130 0.135 0.0900 0.118 0.0247 | Slope (1/n) Y-intercept (log K) Coefficient of Determination (r²) | 0.589 -0.602 0.971 |
| 0.156 mg/L | 0.00493 | 0.0247 | п К Кос | 1.70 0.250 32.7 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.142 0.140 0.140 0.141 0.00106 | 0.0700 0.0800 0.0780 0.0760 0.00529 | | |

^a Concentration in soil-less control

Table VIII. Measured aqueous concentrations, calculated soil concentrations and linear regression results for desorption of 2,4-DP-p from Georgia sand during isotherm testing.

| | | 0.1.1.1.1.0 | <u> </u> | |
|---|--|---|--|-------------------------|
| Initial | Measured Aqueous | Calculated So | | |
| Concentration ^a | Concentration | Concentration | 1 | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.22 mg/L ^b | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.110 0.109 0.112 0.110 0.00153 | 0.124 0.00950 -0.760° 0.0665 NR | | |
| 0.620 mg/L | | | LOG (C ₁) | LOG (Cd) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0580 0.0570 0.0570 0.0573 0.000577 | 0.0790 0.0837 0.0743 0.0790 0.00475 | -1.24 -1.55 -1.90 | -1.10 -1.25 -1.29 |
| 0.309 mg/L | | | Slope (1/n) Y-intercept (log K) | 0.279 -0.776 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0290 0.0280 0.0270 0.0280 0.001 | 0.0630 0.0725 0.0345 0.0567 0.0198 | Coefficient of Determination (r ²) | 0.888 |
| 0.156 mg/L | 0.001 | 0.0196 | n K` K`oc | 3.59 0.167 21.9 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0130 0.0125 0.0122 0.0126 0.000404 | 0.0438 0.0556 0.0552 0.0515 0.00672 | | |

^a Concentration in soil-less control.

^b The results from this concentration were omitted from regression analysis because of the low calculated soil concentration.

^c Value was excluded from calculation of mean.

Table IX. Measured aqueous concentrations, calculated soil concentrations and linear regression results for adsorption of 2,4-DP-p to Sandy loam during isotherm testing.

| Intial | Measured Aqueous | Calculated So | . <u> </u> | |
|---|---|--|---------------------------------------|--------------------------------------|
| Concentration ^a | Concentration | Concentration | | |
| | | (mg/kg) | • | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.216 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.928 0.913 0.896 0.912 0.0160 | 1.44 1.51 1.60 1.52 0.0801 | | |
| 0.620 mg/L | | | LOG (Ce) | LOG (Cs) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.444 0.456 0.431 0.444 0.0125 | 0.880 0.820 0.945 0.882 0.0625 | -0.0398 -0.353 -0.664 -0.977 | 0.181 -0.0547 -0.336 -0.597 |
| 0.309 mg/L | | | Slope (1/n) Y-intercept (log K) | 0.838 0.225 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.219 0.218 0.213 0.217 0.00321 | 0.450 0.455 0.480 0.462 0.0161 | Coefficient of Determination (r²) | 0.999 |
| 0.156 mg/L | 0.00021 | 5.5161 | n K Koc | 1.19 1.68 81.5 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.106 N/A 0.105 0.105 0.000778 | 0.250 N/A 0.255 0.253 0.00389 | | |

^a Concentration in soil-less control

Table X. Measured aqueous concentrations, calculated soil concentrations and linear regression results for desorption of 2,4-DP-p from Sandy loam isotherm testing.

| Initial | Measured Aqueous | Calculated So | | |
|---|---|--|--|---------------------------------------|
| Concentration ^a | Concentration | Concentration | · | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.216 mg/L | (11.3.1) | <u> </u> | , | |
| 1.2 10 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.210 0.214 0.213 0.212 0.00208 | 0.959 1.01 1.09 1.02 0.0659 | | |
| 0.620 mg/L | | | LOG (C ₁) | LOG (Cd) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.117 0.102 0.101 0.107 0.00896 | 0.576 0.589 0.706 0.624 0.0717 | -0.673 -0.972 -1.30 -1.65 | 0.00817 -0.205 -0.462 -0.688 |
| 0.309 mg/L | 0.0520 | 0.326 | Slope (1/n) Y-intercept (log K) Coefficient of Determination | 0.717 0.487 0.999 |
| Replicate 1 Replicate 2 Replicate 3 Mean | 0.0470 0.0510 0.0500 | 0.352 0.357 0.345 | (r ²) | 0.333 |
| Standard Deviation 0.156 mg/L | 0.00265 | 0.0170 | n K' K'oc | 1.40 3.07 149 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0211 NA 0.0234 0.0223 0.00163 | 0.208 NA 0.203 0.205 0.00382 | | |

^a Concentration in soil-less control

Table XI. Measured aqueous concentrations, calculated soil concentrations and linear regression results for adsorption of 2,4-DP-p to Timmerman sandy loam during isotherm testing.

| Intial Concentration ^a (mg/L) | Measured Aqueous Concentration (mg/L) | Calculated So Concentratio (mg/kg) | | |
|---|---|--|---|-------------------------------------|
| 1.22 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 1.12 1.14 1.14 1.13 0.0146 | 0.500 0.365 0.385 0.417 0.0729 | | |
| 0.620 mg/L | | | LOG (Ce) | LOG (Cs) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.565 0.558 0.563 0.562 0.00361 | 0.275 0.310 0.285 0.290 0.018 | 0.0541 -0.250 -0.548 -0.846 | -0.380 -0.538 -0.886 -1.17 |
| 0.309 mg/L Replicate 1 Replicate 2 Replicate 3 Mean | 0.284 0.278 0.287 0.283 | 0.155 0.110 0.130 | Slope (1/n) Y-intercept (log K) Coefficient of Determination (r²) | 0.9075 -0.383 0.979 |
| Standard Deviation 0.156 mg/L | 0.00458 | 0.0229 | n K Koc | 1.10 0.414 78.2 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.141 0.146 0.141 0.143 0.00301 | 0.0750 0.0500 0.0770 0.0673 0.0150 | | |

^a Concentration in soil-less control

Table XII. Measured aqueous concentrations, calculated soil concentrations and linear regression results for desorption of 2,4-DP-p from Timmerman sandy loam during isotherm testing.

| Initial | Measured Aqueous | Calculated So | | |
|---|---|--|------------------------------------|-------------------------------------|
| Concentration ^a | Concentration | Concentration | n | |
| (mg/L) | (mg/L) | (mg/kg) | | |
| 1.22 mg/L | | | | |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.113 0.106 0.0940 0.104 0.00961 | 0.396 0.303 0.377 0.359 0.0489 | | |
| 0.620 mg/L | | | LOG (C ₁) | LOG (Cd) |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0580 0.0540 0.0540 0.0553 0.00231 | 0.219 0.269 0.246 0.245 0.0255 | -0.982 -1.26 -1.57 -1.91 | -0.445 -0.611 -0.948 -1.20 |
| 0.309 mg/L | | | Slope (1/n) Y-intercept (log K) | 0.839 0.399 |
| Replicate 1 Replicate 2 Replicate 3 Mean | 0.0260 0.0250 0.0290 0.0267 | 0.111 0.144 0.0835 0.113 | Coefficient of Determination (r²) | 0.991 |
| Standard Deviation 0.156 mg/L | 0.00208 | 0.0301 | n K` K`oc | 1.19 2.51 474 |
| Replicate 1 Replicate 2 Replicate 3 Mean Standard Deviation | 0.0114 0.0117 0.0140 0.0124 0.00142 | 0.0751 0.0506 0.0650 0.0636 0.0123 | | · <u> </u> |

^a Concentration in soil-less control

Radioactive material balance for 2,4-DP-p using Arkansas clay. Table XIII.

| | DPM in | Total DPM | DPM in | Total DPM | DPM in | | Total DPM | | |
|-----------|-----------------|-------------------------|---------------|-------------------------|-----------------------|------------|-----------|-----------|------------|
| | Adsorption | in Solution | Desorption | in Solution | Extract | Total DPM | in Soil | Total DPM | |
| Rep. | (5 ml) | Adsorption ^b | (5 ml) | Desorption ^b | (5 ml) ^{b,c} | Extraction | Burns | Recovered | % Recovery |
| Initial o | concentration 1 | .22 mg/L (dpm | 554000), bas | sed on soil-less | control | | | | |
| | | • • • • | • | | | | | | |
| 1 | 58700 | 423000 | 9650 | 69500 | 2100 | 15100 | 31800 | 539400 | 97.4 |
| 2 | 60000 | 432000 | 10100 | 72700 | 2210 | 15900 | 30600 | 551000 | 99.5 |
| 3 | 59900 | 432000 | 10500 | 75400 | 2360 | 17000 | 32900 | 557000 | 100.5 |
| Initial o | concentration 0 | .620 mg/L (dpr | n 282000), ba | ised on soil-les | s control | | | | |
| 1 | 31900 | 229000 | 5020 | 36200 | 1150 | 8270 | 20400 | 294000 | 104.4 |
| 2 | 29400 | 212000 | 5570 | 40100 | 1180 | 8500 | 20100 | 280000 | 99.5 |
| 3 | 29300 | 211000 | 5580 | 40200 | 1180 | 8470 | 20500 | 280000 | 99.3 |
| initial o | concentration 0 | .309 mg/L (dpr | n 140000), ba | ised on soil-les | s control | | | | |
| 1 | 15100 | 109000 | 2310 | 16700 | 472 | 3400 | 13600 | 142000 | 101.4 |
| 2 | 14300 | 103000 | 2510 | 18100 | 500 | 3600 | 11900 | 137000 | 97.6 |
| 3 | 14900 | 107000 | 2140 | 15400 | 443 | 3200 | 12000 | 138000 | 98.1 |
| Initial o | concentration 0 | .156 mg/L (dpr | n 70800), bas | ed on soil-less | control | | | | |
| 1 | 7400 | 53300 | 874 | 6300 | 164 | 1180 | 9530 | 70300 | 99.3 |
| 2 | 7370 | 53100 | 958 | 6900 | 189 | 1360 | 8290 | 69600 | 98.4 |
| 3 | 7220 | 52000 | 905 | 6520 | 173 | 1240 | 8980 | 68700 | 97.1 |

^a Calculated values are based on unrounded data rather than the rounded numbers presented here. Apparent

errors in calculation may result from using rounded values.

b Total volume in test system 40 mL

c In order to ensure that adequate material balance would be obtained in the clay soil, the soil was further extracted with 0.01M CaCl₂ and the soil was subsequently combusted for [14C]residues

Table XIV. Radioactive material balance for 2,4-DP-p using Georgia sand. a

| | DPM in | Total DPM | DPM in | Total DPM | DPM in | | Total DPI | VI | |
|---------|---------------|----------------|-------------|--------------------------------|-----------|------------|-----------|-----------|------------|
| | Adsorption | in Solution | Desorption | in Solution | | Total DPM | in Soll | Total DPM | |
| Rep. | (5 ml) | Adsorption b | (5 ml) | <u>Desorption</u> ^t | (5 ml) | Extraction | Burns | Recovered | % Recovery |
| Initial | concentration | n 1.22 mg/L (d | ipm 554000) | , based on | soil-less | control | | | |
| 1 | 64900 | 494000 | 6230 | 47300 | NA | NA | NA | 541000 | 97.6 |
| 2 | 66400 | 504000 | 6180 | 47000 | NA | NA | NA | 551000 | 99.5 |
| 3 | 67200 | 511000 | 6390 | 48500 | NA | NA | NA | 559000 | 101.0 |
| Initial | concentration | n 0.620 mg/L (| (dpm 282000 |)), based on | soil-less | s control | | | |
| 1 | 32800 | 249500 | 3300 | 25100 | NA | NA | NA | 275000 | 97.5 |
| 2 | 32800 | 249400 | 3240 | 24600 | NA | NA | NA | 274000 | 97.2 |
| 3 | 32900 | 250000 | 3220 | 24500 | NA | NA | NA | 275000 | 97.4 |
| Initial | concentration | n 0.309 mg/L (| (dpm 140000 |)), based on | soil-less | s control | | | |
| 1 | 16000 | 122000 | 1640 | 12500 | NA | NA | NA | 134000 | 95.9 |
| 2 | 16000 | 122000 | 1570 | 11900 | NA | NA | NA | 133000 | 95.2 |
| 3 | 16500 | 125000 | 1540 | 11700 | NA | NA | NA | 137000 | 97.8 |
| Initial | concentration | n 0.156 mg/L (| (dpm 70800) | , based on s | oil-less | control | | | |
| 1 | 8040 | 61130 | 738 | 5610 | NA | NA | NA | 66700 | 94.3 |
| 2 | 7930 | 60200 | 709 | 5390 | NA | NA | NA | 65600 | 92.7 |
| 3 | 7970 | 60600 | 691 | 5250 | NA | NA | NA | 65800 | 93.0 |

^a Calculated values are based on unrounded data rather than the rounded numbers presented here. Apparent errors in calculation may result from using rounded values.

b Total volume in test system 40 mL

NA Not applicable. The extraction and combustion steps were not performed with the Georgia sand soil since adequate material balance was obtained after the desorption step.

Table XV. Radioactive material balance for 2,4-DP-p using Sandy loam. a

| Rep. | DPM in Adsorption (5 ml) | Total DPM in Solution Adsorption ^b | DPM in Desorption (5 ml) | Total DPM in Solution Desorption ^b | DPM in Extract (5 ml) ^{b,c} | | Total DPM in Soil Burns | Total DPM Recovered | % Recovery |
|-------------|--------------------------------|---|--------------------------------|---|--|-------|-------------------------------|---------------------------|---------------|
| Initial co | ncentration 1.2 | 22 mg/L (dpm | 554000), ba | sed on soil-le | ss contro | | | | |
| 1 | 52700 | 379000 | 11900 | 85800 | 3430 | 24700 | 49600 | 540000 | 97.4 |
| | 51800 | 373000 | 12100 | 87400 | 3580 | 25800 | 59800 | 546000 | 98.6 |
| 2 3 | 50800 | 366000 | 12100 | 87000 | 3580 | 25800 | 55800 | 535000 | 96.5 |
| Initial co | ncentration 0.6 | 320 mg/L (dpm | n 282000), b | ased on soil-l | ess contr | rol | | | |
| 1 | 25200 | 182000 | 6620 | 47600 | 1910 | 13800 | 35500 | 279000 | 98.8 |
| 2 | 25900 | 186000 | 5780 | 41600 | 1640 | 11800 | 34100 | 274000 | 97.2 |
| 2 3 | 24500 | 176000 | 5720 | 41200 | 1690 | 12100 | 42900 | 272000 | 96.6 |
| Initial co | ncentration 0.3 | 809 mg/L (dpm | n 140000), b | ased on soil-l | ess contr | ol | | | |
| 1 | 12400 | 89400 | 2940 | 21100 | 903 | 6500 | 19100 | 136000 | 97.1 |
| | 12400 | 89100 | 2650 | 19100 | 867 | 6250 | 19500 | 134000 | 95.5 |
| 2 3 | 12100 | 87000 | 2880 | 20700 | 862 | 6200 | 20800 | 135000 | 96.2 |
| Initial cor | ncentration 0.1 | 56 mg/L (dpm | 1 70800), ba | sed on soil-le | ss contro | I | | | |
| 1 | 6040 | 43500 | 1200 | 8610 | 384 | 2760 | 16000 | 70900 | 100 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| 3 | 5960 | 42900 | 1330 | 9580 | 381 | 2740 | 13200 | 68400 | 96.6 |

^a Calculated values are based on unrounded data rather than the rounded numbers presented here. Apparent errors in calculation may result from using rounded values.

^b Total volume in test system 40 mL

^c In order to ensure that adequate material balance would be obtained in the sandy loam soil, the soil was further extracted with 0.01 M CaCl₂ and the soil was subsequently combusted for [¹⁴C]residues.

Radioactive material balance for 2,4-DP-p using Timmerman sandy loam. a Table XVI.

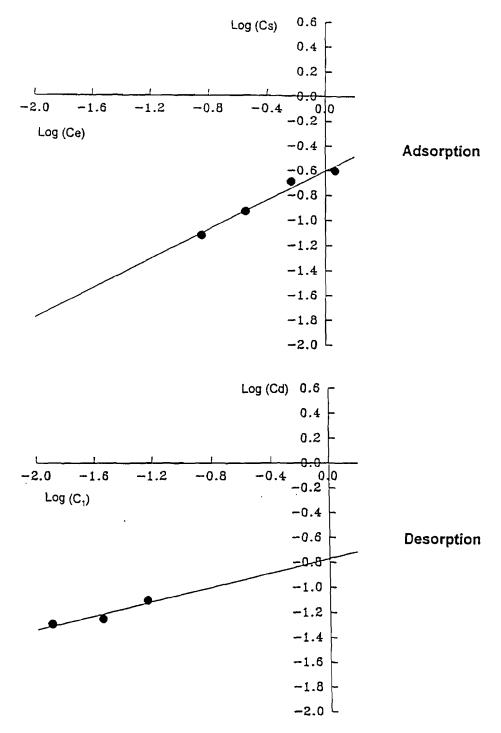
| Rep. | DPM in Adsorption (5 ml) | Total DPM in Solution Adsorption ^b | DPM in Desorption (5 ml) | Total DPM in Solution Desorption ^b | DPM in Extract (5 ml) | Total DPM Extraction | Total DPM in Soil Burns | Total DPM Recovered | % Recover |
|-------------|--------------------------------|---|--------------------------------|---|-----------------------------|-------------------------|-------------------------------|---------------------------|----------------|
| Initial co | ncentration 1.2 | 22 mg/L (dpm | 554000), ba | sed on soil-le | ss contro | ı | , | | |
| 1 | 63400 | 469000 | 6390 | 47300 | NA | NA | NA | 516000 | 93.2 |
| 2 | 64900 | 480000 | 6040 | 44700 | NA | NA | NA | 525000 | 94.7 |
| | 64700 | 478000 | 5330 | 39400 | NA | NA | NA | 518000 | 93.5 |
| Initial cor | ncentration 0.6 | 620 mg/L (dpr | n 282000), b | ased on soil- | less cont | rol | | | |
| 1 | 32100 | 237000 | 3310 | 24500 | NA | NA | NA | 262000 | 92.9 |
| 2 | 31700 | 234000 | 3090 | 22900 | NA | NA | NA | 257000 | 91.3 |
| 3 | 32000 | 237000 | 3080 | 22800 | NA | NA | NA | 260000 | 92.1 |
| Initial cor | ncentration 0.3 | 09 mg/L (dpm | n 140000), ba | ased on soil-l | ess contr | rol | | | |
| 1 | 16100 | 119000 | 1480 | 11000 | NA | NA | NA | 130000 | 92.9 |
| 2 | 15800 | 117000 | 1420 | 10500 | NA | NA | NA | 127000 | 90.8 |
| 2 3 | 16300 | 121000 | 1630 | 12100 | NA | NA | NA | 133000 | 94.7 |
| Initial cor | ncentration 0.1 | 56 mg/L (dpm | n 70800), bas | sed on soil-le | ss contro | I | | | |
| 1 | 8020 | 59300 | 645 | 4770 | NA | NA | NA | 64100 | 90.6 |
| 2 | 8280 | 61300 | 662 | 4900 | NA | NA | NA | 66200 | 93.5 |
| 2 3 | 7980 | 59100 | 793 | 5870 | NA | NA | NA | 64900 | 91.8 |

^a Calculated values are based on unrounded data rather than the rounded numbers presented here. Apparent errors in calculation may result from using rounded values.
b Total volume in test system 40 mL

NA Not applicable. The extraction and combustion steps were not performed with the Timmerman sandy loam soil since adequate material balance was obtained after the desorption step.

Figure 1. Chemical structure of (R)-2-(2,4-Dichlorophenoxy)propionic acid-(phenyl-U-¹⁴C) (2,4-DP-p).

Figure 11. Adsorption and desorption isotherms of 2,4-DP-p in Georgia sand.



2.4.2 Test Conditions. The test containers used for this study consisted of 50-mL Pyrex® glass centrifuge tubes with Teflon®-lined caps. The amounts of soil and water used were selected so as to fill the test vessels completely to avoid possible volatilization of test material. Individual test containers were identified by project number, test material name, replicate number, test phase, and nominal concentration. All test containers were shaken on a Labline Orbital Shaker in an environmental chamber designed to maintain a constant temperature of 20 ± 2 °C.

2.5 Calculation of Aqueous Concentrations

The calculation used in determining the concentration of ¹⁴C-residues in the aqueous test solutions and samples was:

| Test material | naterial (mg/L) = | Net dpm | | | | | |
|-----------------|-------------------|---|--|--|--|--|--|
| 1 GOT THE COTOR | | effective specific activity of 14C-material x sample size | | | | | |

where

Net dpm

disintegrations per minute calculated by the instrument after background subtraction and correction for counting efficiency

Sample size

Sample volume (L)

Effective specific activity

1.14 x 10⁷ dpm/mg for 2,4-DP-p (after isotopic

dilution into dosing stock)

3.0 PRELIMINARY TEST

3.1 Test Solution Preparation

A 2,4-DP-p test solution was prepared for preliminary testing by combining 2.35 mL of the 1.02 mg/mL radiolabeled stock solution and diluting to 2000 mL with sterile 0.01 M CaCl₂. This produced a test solution with a theoretical concentration of 1.20 mg/L. Analysis of the solution in triplicate by liquid scintillation counting resulted in a measured concentration of 1.21 mg/L.

3.2 Preliminary Test Procedure

Preliminary testing was performed to establish solution:soil ratios and equilibration times for the isotherm testing. Testing was performed using the 1.20 mg/L solution of 2,4-DP-p in 0.01 M

CaCl₂ and a 5:1 solution to soil ratio. For each soil, nine test systems containing the test material solution and soil, and nine soil-less controls were established.

For each soil, nine 8-gram (dry weight) aliquots of soil were weighed into 50-mL Pyrex® glass centrifuge tubes with Teffon®-lined caps. A 40-mL aliquot of the solution was then added to each tube, providing a solution to soil ratio of 5:1. In addition, nine centrifuge tubes were prepared containing 40 mL of the test solution to serve as soil-less controls. All tubes were shaken on a Labline Orbital Shaker operating at approximately 125 revolutions per minute (rpm) and were maintained in the dark. Three tubes containing each soil and three soil-less control tubes were removed from the shaker table at intervals of 5, 18, and 24 hours. The tubes were centrifuged (Beckman GSGR centrifuge) at approximately 1000 rpm for 30 minutes to separate the soil and aqueous phases. This centrifuging regime produced a clear supernatant for all soils, with some organic particulate matter (e.g., plant fragments) floating on the surface.

A 5-mL aliquot of the supernatant was removed from each centrifuge tube using a digital pipet with disposable plastic tips and transferred into a scintillation vial. A clean tip was used for each sample. Approximately 15 mL of Monophase® scintillation cocktail was then added to the vials and the contents mixed by shaking. After shaking, the vials were placed into a Packard Tricarb 1600 CA liquid scintillation counter for quantitation of the aqueous concentration of 2,4-DP-p. The results of this analysis were used to establish an equilibrium time (i.e., a plateau in aqueous concentration) and a solution:soil ratio (to result in approximately 50% of the test material in solution following equilibration) for the isotherm test.

3.5 Preliminary Test Analysis

All radioactivity analyses were performed using a Packard Tricarb 1600 CA liquid scintillation counter (LSC) calibrated with factory-prepared standards. Counting efficiencies of all experimental samples were determined using an external standard and a factory-prepared calibration curve (Beckman Instruments). All test samples were counted for a maximum of 5 minutes (Packard LSC) or until a 2 sigma error of 5% was attained. Using this criterion, it was determined at the 90% confidence level that all samples of 31 cpm (background 25.72 cpm) had

an associated error of 10%. This percentage was the maximum acceptable error and was associated with the minimum net cpm of a sample. The counting error decreased as the sample activity increased. The minimum detectable ¹⁴C-residue concentration was dependent on the counting efficiency, sample size (milliliters or grams) and the acceptable minimum net cpm. For [¹⁴C]2,4-DP-p solution prepared using the dosing stock, with an effective specific activity of 11,353.4 dpm/µg, the detection limit using 5-mL aqueous samples and a counting efficiency of 94%, was 0.581 µg/L.

3.4 Preliminary Test Results

Following 5, 18, and 24 hours of agitation, the measured aqueous concentrations of 2,4-DP-p exposed to Arkansas clay were 1.09, 1.04, and 1.05 mg/L, respectively. When exposed to Georgia sand, the measured aqueous concentrations were 1.13, 1.14, and 1.09 mg/L, respectively. Using Sandy loam, the measured aqueous concentrations were 0.943, 0.939, and 0.898 mg/L, respectively, and for using Timmerman sandy loam, the measured aqueous concentrations were 1.11, 1.15, and 1.12 mg/L, respectively (Table II). Graphical presentation of the data (Figures 2 to 5) indicated a plateau in aqueous concentration was established within 5 hours and remained constant through 24 hours. Thus, 18 hours was selected as an equilibrium time for the adsorption phase of the isotherm test. Because little of the test material sorbed to the soils using a 5:1 solution ratio, that ratio was also used in the isotherm tests.

4.0 STABILITY TEST

4.1 Test Solution Preparation

A 2,4-DP-p test solution was prepared for stability testing by combining 1.15 mL of the 1.02 mg/mL radiolabeled stock solution and diffuting to 1000 mL with sterile 0.01 M CaCl₂. This produced a test solution with a theoretical concentration of 1.20 mg/L. LSC analysis of the prepared solution (in triplicate) resulted in a measured concentration of 1.18 mg/L.

4.2 Stability Test Procedure

A stability test was performed in triplicate in 0.01 M CaCl₂ with solution to soil ratios of 5:1 for 2,4-DP-p to verify that the test material did not degrade during the equilibration periods.

3

Three allquots of each soil (8 g dry weight) were placed in 50-mL Pyrex® glass centrifuge tubes with Teflon®-lined screw-caps. A 40-mL aliquot of the test solution was added to each tube, producing a 5:1 solution:soil ratio. All tubes were shaken on a Labline Orbital Shaker (Model 3590) operating at approximately 125 rpm. After 36 hours of shaking, the tubes were removed and the aqueous phase separated, and the aqueous phase was analyzed by high performance liquid chromatography with radiometric detection (HPLC-RAM). Because a large proportion (70.7 to 96.8%) of the test material was in the aqueous phase, the soil was not analyzed.

4.3 Stability Test Analysis

Aqueous samples were subjected to compound-specific analysis by HPLC-RAM for 2,4-DP-p. Instrumentation consisted of a Waters 510 solvent pump, a Hewlett-Packard Model 1050 autosampler and a Radiomatic Model A 280 radioisotope detector.

The HPLC analysis was conducted using the following instrumental conditions:

Column:

Metachem Spherisorb ODS-2, 250 mm (length) x 4.6 mm (l.D.), PS

5 um

Mobile Phase:

A: 0.1% trifluoroacetic acid in reagent water

B: acetonitrile

Gradient Program:

| Time (min) | <u>A%</u> | <u>B%</u> | Type |
|------------|-----------|-----------|--------|
| Initial | 60 | 40 | NA |
| 20 | 60 | 40 | Linear |
| 30 | 40 | 60 | Linear |
| 31 | 0 | 100 | Linear |
| 36 | 0 | 100 | Linear |
| 37 | 60 | 40 | Linear |

Flow Rate:

1.0 mL/minute

Cocktail Type: Flo-Scint II

3

Cocktail Flow Rate: 3.0 mL/minute Flow Cell Volume: 1000 µL

Injection Volume: 10, 100 or 200 µL

Introduction of samples and standards into the chromatographic system was performed by programmed injection.

4.4 Stability Test Results

Analysis of the prepared test solutions by LSC prior to equilibration resulted in a mean concentration of 1.20 mg/L for the 2,4-DP-p solution. The stability of 2,4-DP-p in Arkansas clay, Georgia sand, Sandy loam and Timmerman sandy loam was demonstrated by the high percent of parent material in the aqueous fractions from each of the soils, 96.6 to 100% of recovered radioactivity (Table III). Representative chromatograms from the aqueous phase samples appear in Figures 6 to 9.

5.0 ISOTHERM TEST

5.1 Test Solution Preparation

2,4-DP-p test solutions were prepared in sterile O.O1 M CaCl₂ at theoretical concentrations of 1.20, 0.600, 0.300, and 0.150 mg/L by combining 1.18, O.600, O.300, and 0.150 mL, respectively, of the 1.02 mg/mL radiolabeled stock solution and diluting to 1000 mL with 0.01 M CaCl₂. The solutions thus prepared were assayed in triplicate by liquid scintillation counting (LSC) in order to verify the concentration prior to use.

5.2 Isotherm Test Procedure

The isotherm test was performed in 0.01 M CaCl₂ with a 5:1 solution to soil ratio for all four soils. An equilibrium time of 18 hours was selected for each soil based on the results of the preliminary test.

Three aliquots (8 g dry weight) of each soil and 40 mL of test solution were added to separate test systems for each solution concentration. In addition, three soil-less controls and three soil blanks were prepared for each sample set. The entire sample set was shaken for

18 hours at approximately 125 rpm, followed by phase separation and sampling for radioassay as described in previous sections. The aqueous phase was carefully decanted from each tube containing soil, and the volume was measured. An effort was made to remove as much water as possible from the soil prior to described in Analysis of samples was conducted using the instruments and conditions described in Section 3.3.

The desorption phase of the test was performed by adding sterile 0.01 M CaCl₂ to all the centrifuge tubes containing each soil. The volume of 0.01 M CaCl₂ added was equal to the average volume recovered from the blank vessels in the adsorption phase. The 2,4-DP-p retained in the soil phase was allowed to desorb from the soil while shaking for 48 hours. The centrifuge tubes were removed from the shaker and the aqueous phase separated and analyzed as previously described.

After LSC analysis of the aqueous desorption solution, adequate material balance for the Georgia sand and Timmerman sandy loam was obtained and no further analysis was conducted with these soils. An additional desorption step was performed with the Arkansas clay and Sandy loam soil to remove further [14C]residues. The aqueous phase from the first desorption step was carefully decanted from each tube containing these two soil types, and the volume was measured. A volume of sterile 0.01 M CaCl₂, equal to the volume removed, was added and remaining 2,4-DP-p was allowed to desorb from the soil by shaking at 125 rpm for 18 hours. The aqueous phase was separated and analyzed as previously described. The soil remaining in the centrifuge tubes was analyzed by soil combustion.

5.3 Soil Combustion

The quantity of [14C]residues in the Arkansas clay and Sandy loam soil was determined by combustion of soil aliquots following the desorption phases of the isotherm testing for the purpose of determining material balance.

Samples were combusted in a Packard Model 307 sample oxidizer, and the resultant ¹⁴CO₂ was trapped in Carbosorb® solution to which Permafluor® scintillation cocktail was added.

K and 1/n were determined using the logarithmic transformation of the Freundlich equation:

$$\log \left[\frac{x}{m} \right] = \log K + \frac{1}{n} \log C_e$$

The descrption coefficient (K') was similarly calculated, substituting C_d for x/m and C_1 for C_e .

The sorption and description coefficients were also expressed as a function of the organic carbon content of the soils as:

where:

%C = the percent organic carbon in the soil = % organic matter/1.7

Radioactive material balance was calculated by adding the dpm recovered from the aqueous phase in both the adsorption and desorption phases, and dpm from combusted soil (bound residues), and dividing by the radioactivity initially applied (based on dpm in soil-less controls).

5.5 Isotherm Test Results

Analysis of the test solutions prior to equilibration resulted in concentrations of 1.20, 0.600, 0.300 and 0.150 mg/L for the 2,4-DP-p test solutions. Corresponding soil-less control concentrations were 1.22, 0.620, 0.309, and 0.156 mg/L, respectively (Table IV). Comparison of the prepared test solution and soil-less control concentrations indicates that adsorption to the glass test vessels and Teflon®-lined caps did not occur.

Using the Arkansas clay, the mean concentrations of 2,4-DP-p remaining in solution following adsorption (C_a) were (in order of descending initial concentration) 1.05, 0.531, 0.260, and

PROTOCOL DEVIATIONS

- 1. The protocol states in section 5.2 that all glassware and the 9.01M CaCl₂ solution will be autoclaved prior to use to minimize the possibility of microbial degradation of the test material. For the preliminary phase of the test glassware was not autoclaved but the 0.01M CaCl₂ solution was sterilized. For the remaining phases of the test the glassware and 0.01M CaCl₂ solution were sterilized by autoclave prior to use.
- 2. The protocol states in section 5.8, paragraph two, that a volume of 0.01M CaCl, solution (equal to the aqueous phase removed after the adsorption phase) is added to the soil. Inadvertently, for each soil type, the volumes added to each soil were 5 mL less than the volume recovered because the volume removed for analysis after adsorption was not added.

These deviations are not expected to alter the results of this study.

SPRINGBORN LABORATORIES, INC.

David Wells 7 May 91 Date Study Director